BAKER (MICHAEL) JR INC BEAVER PA F/6 13/13 NATIONAL DAM INSPECTION PROGRAM, DUBOIS CREEK DAM, (NDI NUMBER --ETC(U: FEB 81 J A DZIUBEK DACW31-61-C-0011 AD-A099 083 UNCLASSIFIED NL OF ! 4. END DTIC



HANNA RIVER BASIN

Dubois Creek, Susquehanna County

PENNSYLVANIA

- Dubois Greek Dam

NDI No. PA 00064 PennDER NO. 58-8

Dam Owner: Keystone Water Company



PHASE I INSPECTION REPORT

NATIONAL DAM INSPECTION PROGRAM

PACW 31-81-C-00/11

prepared for

DEPARTMENT OF THE ARMY

Baltimore District, Corps of Engineers Baltimore, Maryland 21203

prepared by

MICHAEL BAKER, JR., INC.

Consulting Engineers 4301 Dutch Ridge Road Beaver, Pennsylvania 15009

February 1981

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SUSQUEHANNA RIVER BASIN

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DuBOIS CREEK DAM
SUSQUEHANNA COUNTY, COMMONWEALTH OF PENNSYLVANIA
NDI No. PA 00064
PennDER No. 58-8

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PREFACE

This report is prepared under guidance contained in the "Recommended Guidelines for Safety Inspection of Dams," for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I Inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM

DuBois Creek Dam, Susquehanna County, Pennsylvania NDI No. PA 00064, PennDER No. 58-8 DuBois Creek Inspected 28 October 1980

ASSESSMENT OF GENERAL CONDITIONS

DuBois Creek Dam is a "Significant" hazard - "Small" size dam owned and operated by the Keystone Water Company, Hallstead District. The dam was found to be in poor overall condition at the time of inspection.

Hydraulic/hydrologic evaluations, performed in accordance with procedures established by the Baltimore District, Corps of Engineers, for Phase I Inspection Reports, revealed that the spillway will not pass the spillway design flood (SDF) without overtopping the dam. An SDF in the range of the 100-year flood to the 1/2 Probable Maximum Flood (1/2 PMF) is required for DuBois Creek Dam. The 100-year flood was chosen because the dam is on the low end of the "Small" size category based on storage capacity. During the 100-year flood, the dam is overtopped by a maximum depth of 0.86 feet for a total duration of 4.50 hours. The spillway is therefore considered "Inadequate." It is recommended that the owner immediately initiate an engineering study to further evaluate the spillway capacity and develop recommendations for remedial measures to reduce the overtopping potential of the dam.

The inspection revealed certain items of remedial work which should be immediately performed by the owner. Items 1 and 2 below should be completed under the direction of a qualified professional engineer experienced in the design and construction of earth dams and appurtenant structures. These include:

- 1) Initiate an engineering study to further evaluate the spillway capacity in order to develop and implement recommendations for remedial measures to reduce the overtopping potential of the dam.
- 2) Provide upstream closure for the intake.
- Repair the spalled and deteriorated portions of the concrete core wall.

DuBOIS CREEK DAM

- 4) Repair the spillway structure to prevent seepage and undermining.
- 5) Fill the erosion gullies on the dam and reseed the areas.
- 6) Remove the debris and sediment at the left side of the spillway approach channel.

In addition, the following operational measures are recommended to be undertaken by the owner:

- Develop a detailed emergency operation and warning system.
- 2) During periods of unusually heavy rainfall, provide around-the-clock surveillance of the dam.
- When warning of a storm of major proportions is given by the National Weather Service, activate the emergency operation and warning system.

It is further recommended that formal inspection, maintenance, and operational procedures and records be developed and implemented. An emergency drawdown plan should be developed in case emergency drawdown of the reservoir should become necessary. These should be included in a formal maintenance and operations manual for the dam.

Submitted by:

MICHAEL BAKER, JR., INC.

John A. Dziubek, P.E.

Engineering Manager-Geotechnical

Date: 19 February 1981

Approved by:

JOHN A. DZIUZEK

DEPARTMENT OF THE ARMY

BALTIMORE DISTRICT, CORPS OF ENGINEERS

JAMES W. PECK

CDL, Corps of Engineers

District Engineer

Date: 13 MAR 8/



Overall View of Dam from Left Abutment

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PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM DUBOIS CREEK DAM NDI No. PA 00064, PennDER No. 58-8

SECTION 1 - PROJECT INFORMATION

1.1 GENERAL

- a. Authority The Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.
- b. <u>Purpose of Inspection</u> The purpose of the inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 DESCRIPTION OF PROJECT

a. Description of Dam and Appurtenances - DuBois
Creek Dam is a diaphragm earthfill embankment 321
feet long and 22 feet high. The embankment has a
side slope of 3H:1V (Horizontal to Vertical)
downstream and 3H:1V upstream. The upstream face
of the embankment is protected with riprap. The
top of the core wall is 3 feet wide and increases
in width to the base which is socketed 5 feet into
the foundation. The base width is shown on Plate 5
(Appendix E) to be 6 feet. The top of the core
wall extends 3 feet and 5 feet above the upstream
and downstream crests of the embankment, respectively. The crest of the dam is 8 feet wide.

The spillway is located at the left abutment and consists of a broad crested concrete weir. The weir is 113.5 feet long perpendicular to the direction of flow. The spillway training walls extend approximately 3.5 feet above the crest of the spillway and are constructed of both concrete and stone. The floor of the spillway channel consists of large stones grouted in place and extends 64 feet downstream of the crest of the weir.

The outlet works for the dam consist of a submerged intake, a 12 inch cast-iron pipe through the embankment to the chlorinator building at the downstream toe of the embankment, a 10 inch service

line, and a 20 inch blow-off pipe. Both the 10 and 20 inch lines are operated by gate valves housed in the chlorinator building.

- b. Location DuBois Creek Dam is located on DuBois Creek, approximately 2.1 miles southwest of Hartford, Pennsylvania. The structure is located in Liberty Township, Susquehanna County, Pennsylvania and the coordinates of the dam are N 41° 56.4' and W 75° 46.2'. The dam can be located on Franklin Forks, Pennsylvania USGS 7.5 minute topographic quadrangle.
- c. Size Classification The height of the dam is 22 feet. Storage at the top of the dam (Elevation 1085.4 feet Mean Sea Level [ft. M.S.L.]) is 78.0 acre-feet. The dam is therefore in the "Small" size category.
- d. <u>Hazard Classification</u> Loss of life is not likely in the event of failure of DuBois Creek Dam. However, damage will likely occur to one home located 1,000 feet downstream and two additional homes located 3,000 feet downstream of the dam. Therefore, DuBois Creek Dam is classified in the "Significant" hazard category.
- e. Ownership The dam is owned and operated by the Keystone Water Company, Hallstead District, 216 Willow Avenue, Susquehanna, Pennsylvania 18847. Mr. Wallace E. Rhodes is the District Manager.
- f. Purpose of Dam The impoundment created by the dam serves as a water supply source for the Keystone Water Company.
- g. Design and Construction History DuBois Creek Dam was designed by Dunning Engineering Company of Scranton, Pennsylvania in 1905. The contractor and date of construction are not known.
- h. Normal Operational Procedures The reservoir is typically maintained at the spillway crest during the fall, winter and spring, and is drawn down several feet during the summer. The dam is visited every day during fall, winter and spring, and is visited in the summer twice a week.

1.3 PERTINENT DATA

a. Drainage Area (square miles) -

b. Discharge at Dam Site (c.f.s.) -Maximum Known Flood -540 (Tropical Storm Agnes, 1972) Spillway Capacity at Maximum Pool (El. 1085.4 ft. M.S.L.) -2200 c. Elevation (feet above M.S.L.)* -Design Top of Dam -Unknown Minimum Top of Dam -1085.4 Maximum Design Pool -Unknown Spillway Crest -1082.0 Streambed at Toe of Dam -1063.8 Maximum Tailwater of Record -Unknown d. Reservoir (feet) -Length of Maximum Pool (El. 1085.4 ft. M.S.L.) -1065 Length of Normal Pool (El. 1082.0 ft. M.S.L.) -890 e. Storage (acre-feet) Top of Dam (El. 1085.4 ft. M.S.L.) -78 Normal Pool (El. 1082.0 ft. M.S.L.) -50 f. Reservoir Surface (acres) -Top of Dam (El. 1085.4 ft. M.S.L.) -7.4 Normal Pool (El. 1082.0 ft. M.S.L.) -Dam g. Type - Diaphragm earthfill with concrete core wall Total Length (feet) -Height (feet) - Design -Unknown Field -22 Top Width (feet) -8.0 Side Slopes - Upstream -3H:1V

Downstream -

3H:1V

^{*}All elevations referenced to the spillway crest, El. 1082.0 ft. M.S.L., as estimated from Franklin Forks, Pennsylvania USGS 7.5 minute topographic quadrangle map.

Zoning -Impervious Core - None Concrete Core Wall

Cut-off - According to the original report on the dam (dated 11 May 1917), the concrete core wall was extended 5 feet lower than the original streambed.

Drains -

None

h. Diversion and Regulating Tunnel -

None

i. Spillway -

Type - Broad crested weir

Location - Left abutment

Length of Crest Perpendicular to
Flow (feet) - 113.5

Width of Crest Parallel to Flow
(feet) - 3

Crest Elevation (ft. M.S.L.) - 1082.0

Gates - None

Downstream Channel - Rectangular channel with stone and concrete walls. The channel bottom consists of large stones concreted in place.

j. Outlet Works - The outlet works consist of a submerged intake with a 12 inch cast-iron pipe (C.I.P.) through the embankment to the chlorinator building at the downstream toe of the embankment. There is a 20 inch ductile iron pipe blow-off line and a 10 inch C.I.P. service line which lead out of the chlorinator building. The gate valves for both these lines are located in the chlorination building.

SECTION 2 - ENGINEERING DATA

2.1 DESIGM

The information reviewed consisted of the Pennsylvania Department of Environmental Resources' (FennDER, File No. 58-8. This file contained the following information:

- Drawing of the dam by Dunning Engineering Company, dated 1905 (Plate 5).
- 2) The earliest inspection report by the Office of the Water Supply Commission of Pennsylvania, dated 13 July 1916.
- 3) A directive from the Water Supply Commission directing the Hallstead & Great Bend Water Company to improve the spillway to handle a higher discharge rate.
- 4) Plans showing the spillway to be widened from 50 feet to 115 feet, dated 1919 (Plate 3). During the field inspection conducted on 28 October 1980, the spillway was measured to be 113.5 feet wide.
- 5) Post Construction inspection reports and photos. The latest inspection, dated 8 August 1965, reported no serious problems. Several earlier inspection reports indicated problems with the spillway channel collapsing, deterioration of the exposed sections of the concrete core wall, and some seepage along the chlorination building.

2.2 CONSTRUCTION

There is no information available regarding construction of the dam from either the owner or PennDER File 58-8.

2.3 OPERATION

The Keystone Water Company is responsible for all operations and maintenance on the dam.

2.4 EVALUATION

- a. Availability The information used is readily available from PennDER File 58-8.
- b. Adequacy The information available is adequate for a Phase I Inspection of this dam.
- c. Validity There is no reason at the present time to doubt the validity of the available engineering data.

SECTION 3 - VISUAL INSPECTION

3.1 FINDINGS

- a. General The inspection was performed on 28 October 1980. A light rain was falling at the time of inspection. The dam and appurtenant structures were found to be in poor overall condition at the time of inspection. Noteworthy deficiencies observed during the visual inspection are described in the following paragraphs. The complete visual inspection check list, field sketch, top of dam profile and typical cross-section are presented in Appendix A.
- b. Dam Seepage was observed at three locations passing through deteriorated portions of the concrete core wall. The most severe of these locations was near Station 2+85 (see Field Sketch in Appendix A) where approximately 10 gallons per minute (g.p.m.) of seepage was occurring. These seepage areas are the result of progressive deterioration of the exposed areas of the concrete core wall. The seepage has caused erosion gullies and slight irregularities on the downstream face of the dam.
- c. Appurtenant Structures Seepage was observed and heard passing under the weir and spillway channel slab on the left side of the spillway. Progressive undermining and future wash-out of portions of this structure may occur if it is not properly repaired. Seepage was observed exiting from the right spillway training wall at the toe of the embankment. This seepage is presumably from flow in or under the spillway channel slab. Some debris and sediment was present at the left side of the spillway approach channel.

The intake structure was submerged during the inspection. No upstream closure is provided for the outlet pipe which passes through the embankment.

d. Reservoir Area - The reservoir side slopes are relatively steep and heavily wooded. No signs of instability were observed. The watershed is primarily forested. The owner's representative indicated that, at the present time, sedimentation has reduced the reservoir storage volume by approximately one-third.

e. Downstream Channel - The downstream channel has mild slopes through a wide forested valley. Several small wooden bridges are located over the channel but these bridges should not significantly restrict flow. One home is located 1,000 feet downstream of the dam. Two additional homes are located 3,000 feet downstream of the dam. DuBois Creek flows along the northwest edge of Hallstead, Pennsylvania before its confluence with the Susquehanna River.

SECTION 4 - OPERATIONAL PROCEDURES

4.1 PROCEDURES

There are no formal procedures for lowering the reservoir or evacuating the downstream area in case of an impending failure of the dam. It is recommended that formal emergency procedures be adopted, prominently displayed, and furnished to all operating personnel.

4.2 MAINTENANCE OF DAM

Generally, the maintenance procedures followed are adequate; however, a more formal maintenance program and procedures should be developed.

4.3 MAINTENANCE OF OPERATING FACILITIES

The spillway channel is repaired and the blow-off line is cleaned every year. Maintenance is performed on an as-needed basis. It is recommended that a formal operation and preventive maintenance schedule be developed and implemented. An emergency drawdown plan should be developed in case emergency drawdown of the reservoir should become necessary.

4.4 DESCRIPTION OF ANY WARNING SYSTEM IN EFFECT

There is no warning system in the event of a dam failure. An emergency warning system should be developed.

4.5 EVALUATION OF OPERATIONAL ADEQUACY

The current operational features are adequate for the purpose they serve. However, it is recommended that a formal maintenance and operations manual be prepared for the dam.

SECTION 5 - HYDRAULIC/HYDROLOGIC

5.1 EVALUATION OF FEATURES

- a. <u>Design Data</u> No hydrologic or hydraulic design calculations are available for DuBois Creek Dam.
- b. Experience Data The maximum flood of record occurred during Tropical Storm Agnes in 1972, at which time a depth of 1.0 feet over the spillway was reported. This depth gives a calculated flow of approximately 540 c.f.s. through the spillway.
- c. <u>Visual Observations</u> During the visual inspection, no problems were observed which would indicate that the dam and appurtenant facilities could not perform satisfactorily during a flood event.
- d. Overtopping Potential DuBois Creek Dam is a "Small" size "Significant" hazard dam requiring evaluation for a spillway design flood (SDF) in the range of the 100-year flood to the 1/2 Probable Maximum Flood (1/2 PMF). Because the dam is on the low end of the "Small" size category in terms of storage capacity, the 100-year flood was chosen as the SDF.

Using material from "The Hydrologic Study - Tropical Storm Agnes" prepared by the Special Studies Branch, Planning Division, North Atlantic Division, Corps of Engineers, in New York City, December 1975, the peak inflow to the impoundment for the 100-year flood was calculated to be 3750 c.f.s. The hydraulic characteristics of the basin, specifically, the Snyder's unit hydrograph parameters, were obtained from a regionalized analysis conducted by the Baltimore District of the U.S. Army Corps of Engineers. Using these parameters and 1.0 inches initial loss and a constant loss of 0.05 inches/hour, a peak inflow of 3690 c.f.s. was obtained for the 100-year flood. This peak flow is within 2 percent of the peak flow computed previously; therefore, this hydrograph was used for the hydraulic analysis.

The hydraulic capacity of the dam, reservoir, and spillway was then assessed by utilizing the U.S. Army Corps of Engineers' Hydrograph Package, HEC-1 DB.

Analyses of the dam and spillway shows that the dam will be overtopped during the 100-year flood by a maximum depth of 0.86 feet for a total duration of 4.50 hours.

e. Spillway Adequacy - As outlined in the above analyses, the spillway will not pass the SDF without overtopping the dam; therefore, the spillway is considered "Inadequate."

SECTION 6 - STRUCTURAL STABILITY

6.1 EVALUATION OF STRUCTURAL STABILITY

- a. <u>Visual Observations</u> The seepage observed passing through the deteriorated portions of the core wall indicate that repair of the exposed portions of the core wall should be accomplished. Also, the seepage and undermining of the spillway structure is a long-term progressive type problem which should be corrected.
- b. Design and Construction Data Calculations of slope and structural stability were not available for review. The slopes have had a history of satisfactory performance, including occasional drawdown of the reservoir during the summer season. In view of the modest height of the dam and a history of satisfactory performance of its moderate slopes, no further stability analysis is deemed necessary.
- c. Operating Records Nothing in the procedures described by the owner's representative indicates concern relative to the structural stability of the dam.
- d. <u>Post-Construction Changes</u> No changes adversely affecting the structural stability of the dam have been performed.
- e. Seismic Stability The dam is located in Seismic Zone 1 of the "Seismic Zone Map of the Contiguous United States," Figure 1, page D-30, "Recommended Guidelines for Safety Inspection of Dams." This is a zone of minor seismic activity. Therefore, further consideration of the seismic stability is not warranted.

7.1 DAM ASSESSMENT

a. Safety - DuBois Creek Dam was found to be in poor overall condition at the time of inspection.

DuBois Creek Dam is a "Significant" hazard - "Small" size dam requiring an SDF in the range of the 100-year flood to 1/2 PMF. The 100-year flood was chosen as the SDF because the dam is on the low side of the "Small" size category. As presented in Section 5, the spillway and reservoir are not adequate to pass the 100-year flood without overtopping the dam. During the 100-year flood, the dam is overtopped by a maximum depth of 0.86 feet for a total duration of 4.50 hours. Therefore, the spillway is considered "Inadequate."

The core wall, where the seepage was observed exiting through it, should be repaired. Also, the seepage and undermining of the spillway structure will become progressively worse with time and the spillway structure should be repaired.

- b. Adequacy of Information The information available and the observations and measurements made during the field inspection are considered sufficient for this Phase I Inspection Report.
- c. <u>Urgency</u> The owner should immediately initiate the action discussed in paragraph 7.1.d.
- d. Necessity for Additional Data/Evaluation The hydraulic/hydrologic analysis performed for this dam has indicated the need for additional spillway capacity. It is recommended that the owner of DuBois Creek Dam immediately initiate an engineering study to further evaluate the spillway capacity and to develop recommendations for reducing the overtopping potential of the dam.

7.2 RECOMMENDATIONS/REMEDIAL MEASURES

The inspection and review of information revealed certain items of work which should be performed immediately by the owner. Items 1 and 2 should be designed and completed under the guidance of a qualified professional engineer experienced in the design of earth dams and appurtenant structures.

- Initiate an engineering study to further evaluate the spillway capacity in order to develop and implement recommendations for remedial measures to reduce the overtopping potential of the dam.
- 2) Provide upstream closure for the intake.
- 3) Repair the spalled and deteriorated portions of the concrete core wall.
- 4) Repair the spillway structure to prevent seepage and undermining.
- 5) Fill the erosion gullies on the dam and reseed the areas.
- 6) Remove the debris and sediment at the left side of the spillway approach channel.

In addition, the following operational measures are recommended to be undertaken by the owner:

- 1) Develop a detailed emergency operation and warning system.
- During periods of unusually heavy rainfall, provide around-the-clock surveillance of the dam.
- 3) When warning of a storm of major proportions is given by the National Weather Service, activate the emergency operation and warning system.

It is further recommended that formal inspection, maintenance, and operational procedures and records be developed and implemented. An emergency drawdown plan should be developed in case emergency drawdown of the reservoir should become necessary. These should be included in a formal maintenance and operations manual for the dam.

APPENDIX A

VISUAL INSPECTION CHECK LIST, FIELD SKETCH, TOP OF DAM PROFILE, AND TYPICAL CROSS-SECTION

Check List Visual Inspection Phase 1

Coordinates	Long. W 75°46.2'	Temperature 35° F.	1063.83 Tailwater at Time of Inspection <u>ft.*</u> M.S.L.	evel from Franklin Forks, PA
County Susquehanna State PA		Weather Rainy	1082.0 ft.* M.S.L. Tailwater	ssume datum for reservoir l guadrangle map.
Name of Dam DuBois Creek Dam County	NDI # PA 90964 PennDER # 58-8	Date of Inspection 28 October 1980	Pool Elevation at Time of Inspection	*All elevations referenced to assume datum for reservoir level from Franklin Forks, PA U.S.G.S. 7.5 minute topographic quadrangle map.

James G. Ulinski

Recorder

Bruce Juergens, American Water Works Service Co., Inc. Wallace E. Rhodes, Keystone Water Co. William E. Hutcheson, Keystone Water Co.

Owner's Representatives:

Michael Baker, Jr., Inc.:

Inspection Personnel:

James G. Ulinski Wayne D. Lasch Jeff S. Maze

CONCRETE/MASONRY DAMS - Not Applicable

Name of Dam: DUBOIS CREEK DAM NDI # PA 00064 VISUAL EXAMINATION OF OBSERVATIONS	REMARKS OR RECOMMENDATIONS
LEAKAGE	
STRUCTURE TO ABUTMENT/EMBANKMENT JUNCTIONS	
DRAINS	
WATER PASSAGES	
FOUNDATION	

CONCRETE/MASONRY DAMS - Not Applicable

Name of Dam: DUBOIS CREEK DAM NDI # PA 00064	
VISUAL EXAMINATION OF OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS CONCRETE SURFACES	
STRUCTURAL CRACKING	
VERTICAL AND HORIZONTAL ALIGNMENT	
MONOLITIN JOINTS	
CONSTRUCTION JOINTS	

REMARKS OR RECOMMENDATIONS

EMBANKMENT

Name of Dam DUBOIS CREEK DAM

NDI # PA 00064

VISUAL EXAMINATION OF OBSERVATIONS

SURFACE CRACKS

None observed

UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE

None observed

Downstream slope is slightly irregular, probably the result of erosion caused by seepage through the core wall.

SLOUGHING OR EROSION OF EMBANKMENT AND ABUTMENT SLOPES

Fill in erosion gullies and reseed.

EMBANKMENT

Name of Dam DUBOIS CREEK DAM

NDI # PA 00064

REMARKS OR RECOMMENDATIONS Good horizontal and vertical alignment, however, concrete core wall is cracking and spalling. Some voids are present in the concrete core wall. OBSERVATIONS VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST VISUAL EXAMINATION OF

Repair spalled concrete and fill voids in core wall.

RIPRAP FAILURES

None observed

EMBANKMENT

Name of Dam DUBOIS CREEK DAM

NDI # PA 00064

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM	Small amount of erosion along abutments of dam and training wall, along the embankment and abutment, and where water seeps through core wall.	Fill in erosion gullies and seed areas.
ANY NOTICEABLE SEEPAGE	Seepage was observed at the following locations and at the approximate rates: Sta. 1+25 at toe of dam 1.0 g.p.m. Sta. 2+20 at core wall 0.25 g.p.m. Sta. 2+45 at core wall 0.50 g.p.m. Sta. 2+85 at core wall 10.0 g.p.m.	Repair spillway channel. Repair core wall. Repair core wall. Repair core wall.
STAFF GAGE AND RECORDER	None observed	

DRAINS

One drain was observed to the left of the outlet pipe. This drain exits from the chlorinator building. No drains for the embankment were observed.

OUTLET WORKS

Name of Dam: DUBOIS CREEK DAM

NDI # PA 00064

REMARKS OR RECOMMENDATIONS OBSERVATIONS VISUAL EXAMINATION OF

CRACKING AND SPALLING OF

None observed

CONCRETE SURFACES IN

OUTLET CONDUIT

Provide upstream closure for the intake pipe. The intake structure was submerged at No upstream closure was provided for the 12 in. cast iron pipe which passes through the time of inspection. the embankment.

INTAKE STRUCTURE

chlorinator building and valve system downstream. A 20 in. ductile iron pipe blow-off exits into the natural A 12 in. cast iron pipe runs to a

OUTLET STRUCTURE

feeds the water distribution system. streambed and a 10 in. service line No problems observed.

Natural stream channel is in good condition.

OUTLET CHANNEL

None observed

.

EMERGENCY GATE

UNGATED SPILLWAY

Name of Dam: DUBOIS CREEK DAM

NDI # PA 00064

The weir should be repaired to prevent seepage and undermining. Remove debris and sediment. REMARKS OR RECOMMENDATIONS Top of weir varies in height by + 8 in. Seepage passes under weir at the left side. Some debris and sediment is located in the left side of spillway channel. OBSERVATIONS VISUAL EXAMINATION OF APPROACH CHANNEL CONCRETE WEIR

The structure should be repaired to prevent seepage and undermining. Water is seeping through the concrete and stone channel floor and undermining the structure.

DISCHARGE CHANNEL

BRIDGE AND PIERS

S None

1

GATED SPILLWAY - Not Applicable

NDI # PA 00064 REMARKS OR RECOMMENDATIONS REMARKS OR RECOMMENDATIONS	Name of Dam: DUBOIS CREEK DAM
--	-------------------------------

CONCRETE SILL

APPROACH CHANNEL

DISCHARGE CHANNEL

BRIDGE AND PIERS

GATES AND OPERATION EQUIPMENT

INSTRUMENTATION

Name of Dam: DUBOIC COREY D	INSTRUMENTATION	
NDI # PA 00064	Dini.	
VISUAL EXAMINATION	ODSERVATIONS	REMARKS OR RECOMMENDATIONS
Monumentation/surveys	None observed	
OBSERVATION WELLS	None observed	
WBIRS	None observed	
Piezometers	None observed	
OTHER	None	

REMARKS OR RECOMMENDATIONS

RESERVOIR

Name of Dam: DUBOIS CREEK DAM

NDI # PA 00064

VISUAL EXAMINATION OF

SLOPES

The reservoir side slopes are fairly steep (15°-45°), but no signs of instability were observed.

OBSERVATIONS

SEDIMENTATION

The average depth of the reservoir according to the owner is 6 ft. According to the owner's representative, approximately one-third of the original storage volume has been filled in by sedimentation.

DOWNSTREAM CHANNEL

Name of Dam: DUBOIS CREEK DAM

NDI # PA 00064

OBSERVATIONS VISUAL EXAMINATION OF

REMARKS OR RECOMMENDATIONS

(OBSTRUCTIONS, DEBRIS, ETC.) CONDITION

Several No debris was present in the channel. Seven small wooden bridges located on the channel will not restrict heavy flows.

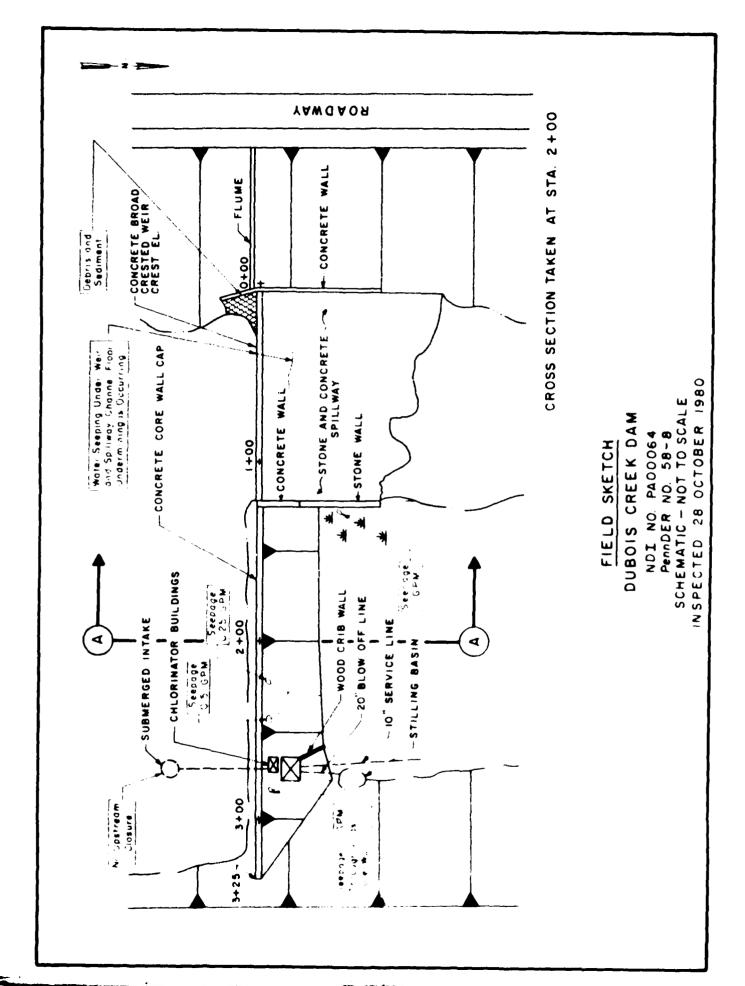
SLOPES

The downstream channel has mild slopes through a wide valley.

APPROXIMATE NO. OF HOMES AND

POPULATION

One home is located 1,000 ft. downstream of the dam. Two additional homes are located 3,000 ft. downstream of the dam.



MICHAEL BAKER, JR., INC. DUBOIS CREEK DAM THE BAKER ENGINEERS TOP OF DAM PROFILE Box 280 TYPICAL CROSS-SECTION Beaver, Pa. 15009 DATE OF INSPECTION: 28 October 1980 * ABUTMENT 3150 MINING TOP OF DAT 1085.4 ELEV. (LOOKING DOWNSTREAM 0450 2100 STATION STATION 321 FEET 0110 ELEV. 1085. 7 FT. SPILLWAY ELEV. 1082.0 FT. HORIZONTAL HORIZON TAL 0430 DAM SECTION PROFILE ELEVATION 1085.4 FT. 00 0750 Longra OF CAM CROSS 0 + 50 700 PPICAL ELEVATION 0 to 1030 0801 (75W 1334; NOILHASTS LERALION (EREL

APPENDIX B

ENGINEERING DATA CHECK LIST

Name of Dam: DUBOIS CREEK DAM ENGINEERING DATA CHECK LIST

REMARKS

NDI # PA 00064

5 and the Field Sketch (page A-13) of this report. A USGS 7.5 minute topographic quadrangle, Franklin Forks, Pennsylvania, was used to prepare the vicinity map which is enclosed in this report as the Location Plan (Plate 1). No construction information available. See Plates 3 and REGIONAL VICINITY MAP CONSTRICTION HISTORY PLAN OF DAM ITEM

See Flate

TYPICAL SECTIONS OF DAM

No information available

HYDROLOGIC/HYDRAULIC DATA

5 and Typical Cross Section (page A-14).

See Plate 3 and the Field Sketch (page A-13) of this report. OUTLETS - PLAN

No information available No information available - CONSTRAINTS DETAILS

No information available DISCHARGE RATINGS The owner keeps weekly pumpage and reservoir level records. RAINFALL/RESERVOIR RECORDS

Name of Dam: DUBOIS CREEK DAM

NDI # PA 00064

REMARKS ITEH

DESIGN REPORTS

No information available

GEOLOGY REPORTS

No information was available. The regional geology is presented as Appendix F of this report.

HYDROLOGY & HYDRAULICS DAM STABILITY SEEPAGE STUDIES DESIGN COMPUTATIONS

No information available

No information available

MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD

POST-CONSTRUCTION SURVEYS OF DAM

None

No information available

BORROW SOURCES

Name of Dam: DUBOIS CREEK DAM
NDI # PA 00064

NDI # PA 00064	
ІТЕМ	REMARKS
MONITORING SYSTEMS	None
MODIFICATIONS	The spillway was enlarged in 1919. Various post-construction repairs of the spillway have been performed on an as-needed basis, including the right side of the spillway in 1928 and the modifications to the lower right training wall in 1937. In 1941, repairs were performed to portions of the exposed core wall of the dam.
HIGH POOL RECORDS	One of the operators of the dam reported during the visual inspection that the reservoir level had come to within one foot of the top of the core wall in the 1940's.
POST-CONSTRUCTION ENGINEERING STUDIES AND REPORTS	No detailed engineering reports other than the 13 July 1916 Water Supply Commission Inspection are available. A number of inspection reports are available in the PennDER file, including the latest recorded inspection on 8 August 1965 by PennDER.
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	None reported

No formal records are maintained.

MAINTENANCE OPERATION RECORDS

Name of Dam: DUBOIS CREEK DAM

SPILLWAY PLAN,

ITEM

See Plates 3, 4, and 5 and the Field Sketch (page A-13) of this report.

REMARKS

SECTIONS, and DETAILS

OPERATING EQUIPMENT PLANS & DETAILS

No information available

CHECK LIST HYDROLOGIC AND HYDRAULIC DATA ENGINEERING DATA

DRAINAGE A	AREA CHARACTERISTICS: 7.77 sq.mi. (primarily forested)
ELEVATION	TOP NORMAL POOL (STORAGE CAPACITY): 1082.0 ft. M.S.L.
	(50 acft.)
ELEVATION	TOP FLOOD CONTROL POOL (STORAGE CAPACITY): 1085.4 ft. M.S.L
	(78 acft.)
ELEVATION	MAXIMUM DESIGN POOL: Unknown
ELEVATION	TOP DAM: 1085.4 ft. M.S.L. (minimum top of dam)
SPILLWAY:	Rectangular channel
a. b. c.	Crest Elevation 1082.0 ft. M.S.L. Type Concrete broad-crested weir Width of Crest Parallel to Flow 3 ft.
đ.	Length of Crest Perpendicular to Flow 113.5 ft.
e. £.	Location Spillover <u>Left abutment</u> Number and Type of Gates <u>None</u>
OUTLET WO	RKS: 12 in. C.I.P. through embankment with 10 in. service
c. d.	Type line and 20 in. blow-off at downstream toe. Location Near right end of dam Entrance Inverts Unknown Exit Inverts 1063.83 ft. Emergency Drawdown Facilities 20 in. ductile iron blow-off pipe
HYDROMETE(DROLOGICAL GAGES: None
	Type Location Records
MAXIMUM NO	ON-DAMAGING DISCHARGE 540 c.f.s.

APPENDIX C

PHOTOGRAPH LOCATION PLAN AND PHOTOGRAPHS

DETAILED PHOTOGRAPH DESCRIPTIONS

- Overall View of Dam View of Dam from Left Abutment
- Photograph Location Plan
- Photo 1 View of Spillway from Left Abutment
- Photo 2 View of Crest of Spillway from Left Abutment
- Photo 3 View of Spillway Chute and Downstream Channel from Left Training Wall
- Photo 4 View of Spillway Outlet Channel from End of Spillway Chute
- Photo 5 View Looking Upstream at Left Half of Spillway Chute
- Photo 6 View Looking Upstream at Right Half of Spillway Chute
- Photo 7 View of Upstream Face of Dam from Left Shoreline of Reservoir
- Photo 8 View Along Crest of Dam from Right Training Wall of Spillway
- Photo 9 View of Downstream Face of Dam from Right Training Wall of Spillway
- Photo 10 View Along Crest of Dam from Right Abutment
- Photo ll Close-up of Hole in Upstream Side of Concrete Core Wall
- Photo 12 View of Downstream Side of Hole in Concrete Core Wall
- Photo 13 View of Seepage Exiting from Hole in Concrete Core Wall
- Photo 14 View of Seep Located in Concrete Core Wall to Left of Valve House Structure
- Photo 15 View of Outlet Conduit Valve House Structure from Downstream

Photo 16 - View of Downstream End of Outlet Conduit

Note: Photographs were taken on 28 October 1980.

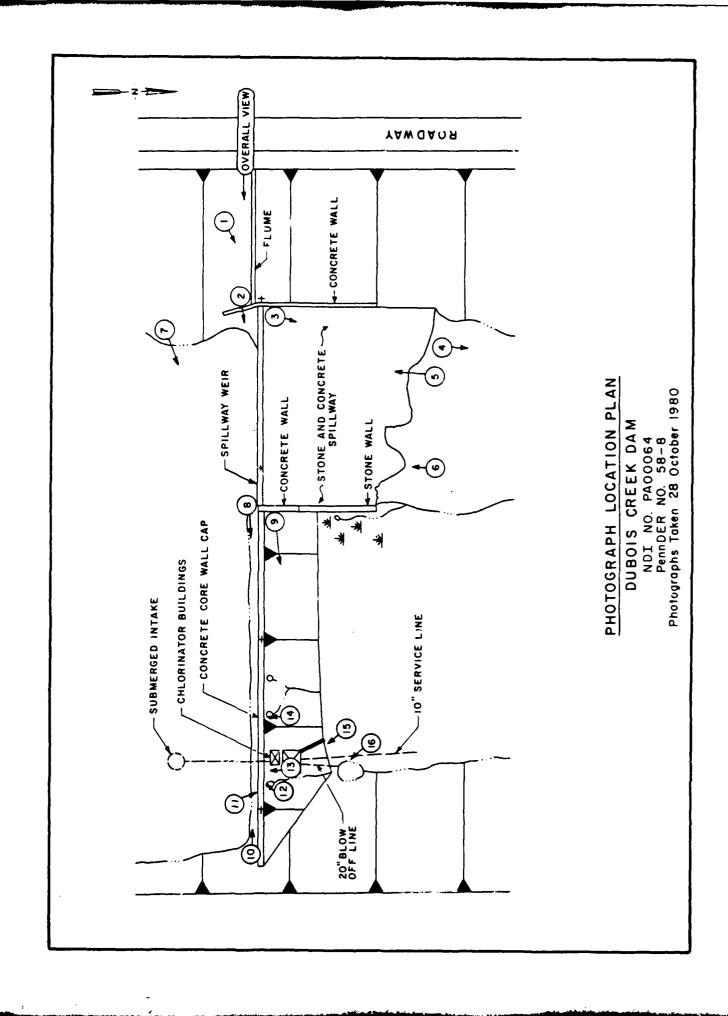




PHOTO 1. View of Spillway from Left Abutment



PHOTO 2. View of Crest of Spillway from Left Abutment



PHOTO 3. View of Spillway Chute and Downstream Channel from Left Training Wall



PHOTO 4. View of Spillway Outlet Channel from End of Spillway Chute



PHOTO 5. View Looking Upstream at Left Half of Spillway Chute

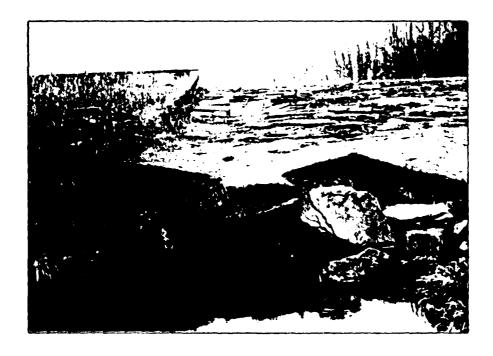


PHOTO 6. View Looking Upstream at Right Half of Spillway Chute



PHOTO 7. View of Upstream Face of Dam from Left Shoreline of Reservoir

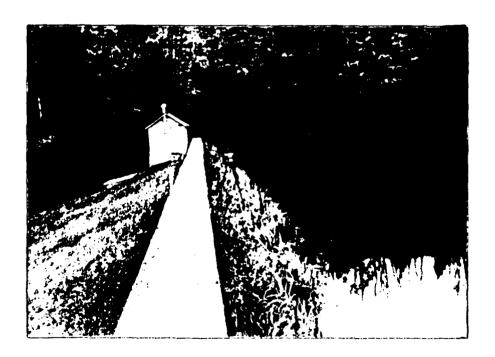


PHOTO 8. View Along Crest of Dam from Right Training Wall of Spillway

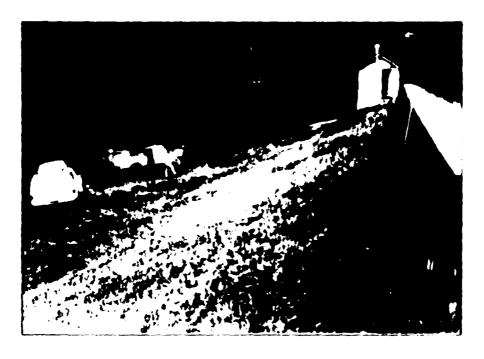


PHOTO 9 View of Downstream Face of Dam from Right Training Wall of Spillway



PHOTO 10 View Along Crest of Dam from Right Abulment

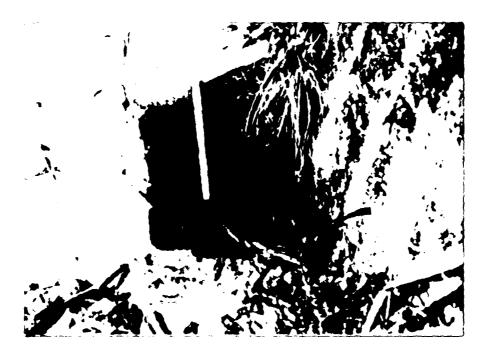


PHOTO 11 Close up of Hole in Upstream Side of Concrete Core Wall-



PHOTO 12 View of Downstream Side of Hole in Concrete Core Wall



PHOTO 13. View of Seepage Exiting from Hole in Concrete Core Wall

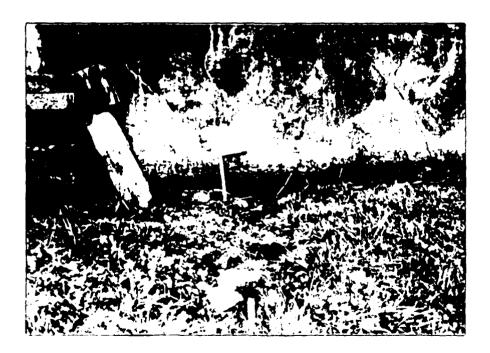


PHOTO 14. View of Seep Located in Concrete Core Wall to left of Valve House Structure



PHOTO 15. View of Outlet Conduit Valve Structure from Downstream

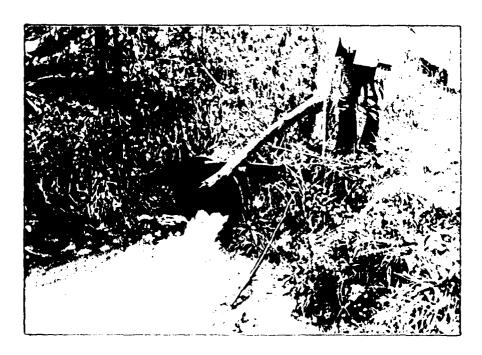


PHOTO 16. View of Downstream End of Outlet Conduit

APPENDIX D

HYDROLOGIC AND HYDRAULIC COMPUTATIONS

The state of the s

MICHAEL BAKER, JR., INC.

THE BAKER ENGINEERS

Box 280 Beaver, Pa. 15009 Subject DUBDIS CREEK DAN S.O. No.

APPENUIX D - HYDROLOGIC Sheet No. of

AND HYDRAULIC SEMPETATIONS Drawing No.

Computed by GNT Checked by Date 2-16-51

SUBJECT	PAGE
PREFACE	i
HYDROLOGY AND HYDRAULIC DATA BASE	1
HYDRAULIC DATA	2
DRAINAGE AREA AND CENTROID MAP	3
TOP OF DAM PROFILE AND CROSS SECTION	4
SPILLWAY DISCHARGE RATING	5
100-YEAR STORM DISTRIBUTION	6
100-YEAR DISCHARGE CALCULATION	7
HEC-1 SPILLWAY CAPACITY ANALYSIS	8

PREFACE

HYDROLOGIC AND HYDRAULIC COMPUTATIONS

The hydrologic determinations presented in this Phase I Inspection Report are based on the use of a Snyder's unit hydrograph developed by the U.S. Army Corps of Engineers. Due to the limited number of gaging stations available in this hydrologic region and the wide variations of watershed slopes, the Snyder's coefficients may yield results of limited accuracy for this watershed. As directed however, a further refinement of these coefficients is beyond the scope of this Phase I Investigation.

In addition, the conclusions presented pertain to present conditions, and the effect of future development on the hydrology has not been considered.

HYDROLOGY AND HYDRAULIC ANALYSIS DATA BASE

NAME OF DAM: DUBOIS CREEK DA	M				
100-YEAR 24 HOUR RAINFALL = 6.	4 INCHES (1)				
STATION	1	2	3	4	٤
Station Description	DUBOIS CREEK DAM				
Drainage Area (square miles)	7.77				
Cumulative Drainage Area (square miles)	7.77	_			
Adjustment of PMF (for Drainage Ares (%)		·———			
6 Hours 12 Hours 24 Hours 48 Hours 72 Hours	100-YEAR STORM DISTRIBUTION ON SHEET 6				
Snyder Hydrograph Parumeters					
Zone (2)	11A				
c _p /c _t (3)	0.62/1.50				
L (miles) (4)	5.19				
L _{ca} (miles) (4)	2.27				
$t_p = C_t (L \cdot L_{ca})^{0.3} \text{ (hours)}$	3.14				
Spillway Data Crest Length (ft) Freeboard (ft) Discharge Coefficient Expanent	113.5 2.7 RATING CURVE DEVELOPED ON SHEET 5				

⁽¹⁾ Technical Paper No. 40, Cooperative Studies Section, U.S. Weather Bureau, Washington, D.C., 1961.

 $^{^{(2)}}$ Hydrological zone defined by Corps of Engineers, Baltimore District, for determining Snycer's Coeff $_{c}$ and $_{c}$ $_{c}$

⁽³⁾ Snyder's Coefficients.

⁽⁴⁾ L = Length of longest water course from outlet to basin divide.

Lca = Length of water course from outlet to point opposite the centroid of drainage area.

MICHAEL BAKER, JR., INC. THE BAKER ENGINEERS

> Box 280 Beaver, Pa. 15009

Subject Desis Creek DAIL S.O. No. HYDI AULIC [174] Sheet No. 2 of 12 Computed by Gillet Checked by Will Date 12-2-33

STORAGE CALCULATIONS

FREA VS. ELEVATION DATA (MEASURED FROM QUAD)

ELEVATION (FT)	SURFACE PREA	(ACRES)
1082	7. 35	
1100	18.37	
1120	54.18	
	l .	

NOPMAL POOL STORAGE

STORAGE VOLUME = VN = 1/3 (A, + A, +VA, A)

h = ESTIMATED AVERAGE DEPTH - 7 FT.

A, = SURFACE AREA OF NORMAL POOL = 7.35 Ac.

A SURFACE AREA OF RESERVOIR BOTTOM = 7.03 AL. (ESTIMATED FROM AVERAGE DEPTH

AND RESERVOIR SIDE SLOPES)

NORMAL POOL STORAGE = VNP = 1/3 (7.35 + 7.03 + V(7.35) 7.03) Van = 50.32 Ac. - FT.

TOP OF DAM STORAGE

78 AC,-Fr. (FROM HEC-1 ANALYSIS)

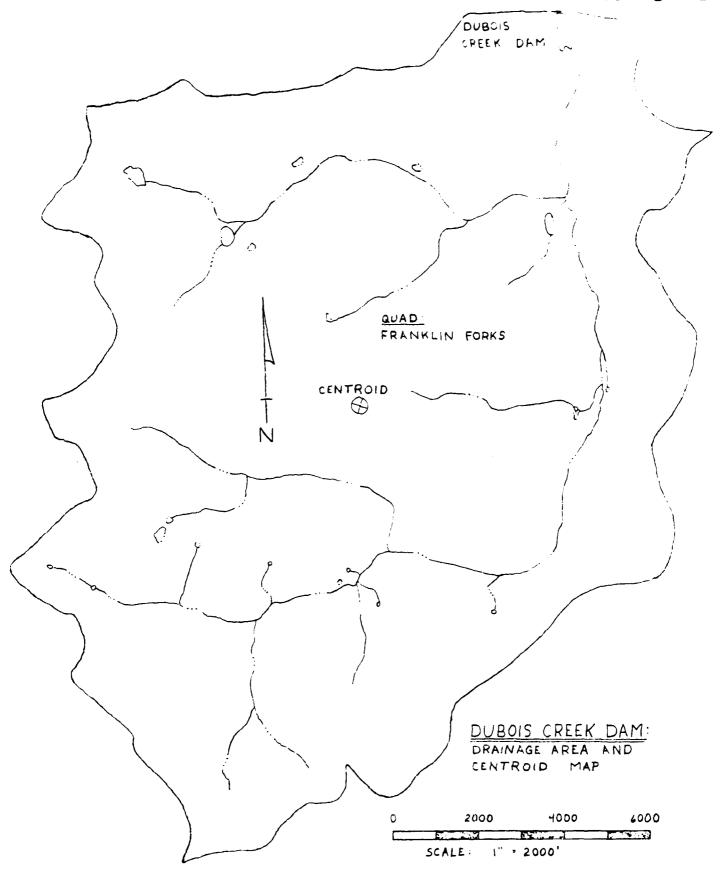
SNYDER'S UNIT HYDROGIAPH PARAMETERS

L=5.19 M., La = 2.27 M.

WATERSHED IS IN ZONE IIA

C,= 0.62 , C. 1.50 t,= 1,50 (L×Lc,) = 3.14 Hx.

DRAINAGE AREA : 7.77 Sq. Mi.



MICHAEL BAKER, JR., INC.		S CREEK DAM	
THE BAKER ENGINEERS		M PROFILE	
Box 280		CROSS SECTION	
Beaver, Pa. 15009	Computed by	WT_Checked by RUS	Date 11/14/80
TOP OF DAM PROFILE (LOOKING DOWNSTREAM) LENGTH OF DAM = 32/ FEET MINIMIN TOP OF DAM ELEV. 1085.7 FT. ELEV. 1085.7 FT.	1080 Abunation DAM Abunation DAM Apolitical LEV.: 1082.0 Ft. DAM Abunation 2400 3400 3450 HORIZON TAL STRTION	FELEVATION FORS. 1 FT. SELEVATION FORS. 1 FT. SOBO CEET of DAM. CEET of DAM.	1070 0400 0400 0400 0400 0400 0450 HORIZONTAL STRTION
(75W 1333)	/*V/14011313	LEVATION (REET MSL)	1

MICHAEL BAKER, JR., INC.

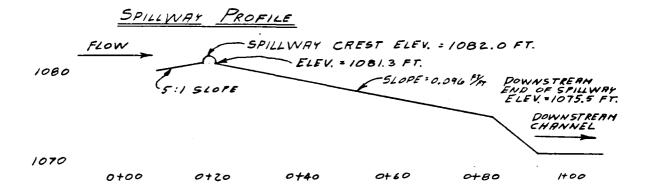
THE BAKER ENGINEERS

Subject Pubois CREEK DAM S.O. No. 13E37-00-ARA-02

SPILLWAY DISCHARGE RATING Shoot No. 5 of 12

Box 280 Beaver, Pa. 15009

__ Drawing No. __ Computed by GUT __ Checked by _____ AUD __ Date _//-20-80



DEVELOP RATING CURVE BASED UPON CRITICAL FLOW OVER SPILLWAY:

V= 49D (CHOW, OPEN CHANNEL HYDRAULICS P. 43

9 = 32.2 FT/SEC. "

D: MEAN HYPANULIC DEPTH : FREE SURALE TOPWIDTH = T

V. MEAN FLOW VELOCITY

Q = AV

SPILLWRY ELEVATION, FT.	FLOW DEPTH,	AREA Fr2	TOP WIDTH,	Ry	V, FT/SEC	Q, CF5	1/20	RESERVOIR SURFACE, FT.
1082.0	0	0	0	0	0	0	0	1082.00
1082.5	0.5	43.75	107.5	.41	3.63	158.81	0.20	1082.70
1083.0	1.0	100.50	113.5	.89	5. 35	537,68	0.44	1083,44
1083.5	1.5	157.25	1/3.5	1.3e	6,66	1,047.29	0.69	1084.19
1084.0	2.0	214.00	113.5	1.88	7.78	1,664.92	0,94	1084.94
1084.5	2,5	270.75	1/3.5	2,38	8.75	2,369.06	1.19	1085.69
1004.7	2.7	327.50	1/3.5	2.89	9.65	3,160.38	1.45	1086.15
1085.2	3, 2	384,63	115.0	3,34	10,37	3,980.61	1.67	1086.87
1085.7	3, 7	442.63	117.0	3,78	11.03	1,862.21	1.89	1087.59
1086.0	4.0	501.63	119.0	1,22	11.66	5,019.01	2.11	1088.11
1086.5	4.5	561.63	121.0	9.64	12.22	6,863.12	2.32	1088.82
1087.5	5.5	684,63	123.0	5.57	13.39	9,168.78	2.78	1090, ZB
1088.5	6.5	809.63	125.0	6.48	14.44	11,695.05	3. 24	1091.74

Box 280 Beaver, Pa. 15009 Computed by GULT Checked by US Date 1/-25-80 100-YR. RAINERS FROM. TP. 40: 2 H		100-4EAR 5	. 2007	_ Sheet No. 6 of 12
Beaver, Pa. 15009 Computed by GUT Checked by U) Date 11-15-80 Da	Box 280			
100 - YR RAINFALL FIROURY FROM TP-40: 30 MIN. 2.5 JM 3 ML 5.3 JM 3 ML 5.5 JM 1 ML 5.5 JM 1 ML 5.5 JM 1 ML 6.5 JM 1 ML		Computed by	Checked by Link	Date 11-25-80
100-YR RAINFALL AIROUNTS FROM TP-40: 36 ATM 25 ATM 3 ATM				
RAMERIL PRODUCT FROM 36 HIN 21 IN 3 HE. 25 IN 3 HE. 25 IN 4 HE. 45 IN 12 HE 55 IN 14 HE 55 IN 15 HE 55 IN 16 HE 55 IN 16 HE 55 IN 17 HE 56 A IN 18 HE 56 A IN 18 HE 56 A IN 19 HE 56 A IN 10 HE 56 A IN 1	0		2.1	
RAINFALL PRODUCTS FROM 30 Min 21 Ju 1 ML 21 Ju 2 HL 25 Ju 3 HL 3,5 Ju 4 HL 4,5 Ju 12 HL 55 Ju 24 HL 55 Ju 24 HL 56 4 Ju 26 Ju 27 Ju 28 Ju 29 Ju 20 Ju	100-48	de la company de		The second secon
36 MM : 2.1 Mm . 3.3 Mm . 3 MM . 3.4 Mm . 3.5 Mm . 3 MM		PROUNTS FROM	TP-40:	en como e marca e a suma como como e a sua como como como como como como como com
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3 HR. 3.6 IN. 6 HR. 4,5 IN. 12 HR. 5.5.7 IN. 24 HR. 6.4 IN. 25.5 IN. 26 HR. 6.4 IN. 27 O.25 20.1	<i>y</i> 1			
12 HE 5.5 IN. 0]	
24 HR : 6.4 JW. 25 C.25 C.25 20.15 C.083 20.15 C.083 20.037 20.16 C.083 20.037 20.17 C.083 20.037 20.18 C.083 20.037 20.083	6 HR	; 4,5 /N.		
0 14 HR : 6.4 JW. 0 24 HR : 6.4 JW. 0 25 Co.25 0 0.15 0 0.05 0 0.05 0 0.037 0 0 0.037 0 0 0.037 0 0 0.037 0 0 0.037 0 0 0 0.037 0 0 0 0.037 0 0 0 0 0.037 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	IL HR	· 5.5 /w		
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			0.15	and the contract of the contra
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TIME, HRS. RAINFALL DISTRIBUTION: [30 MINUTE INTERVALS] JIMTERVAL NUMBERS			<u>-</u>	and the second s
RAINFALL DISTRIBUTION	-0-1-4-6-	810-12-14-	16-18-20-22-24	management on the control of the con
RAINFALL DISTRIBUTION		TIME HRS.		
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JNTERVAL NUMBERS			The second control of	
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32.8 34 5.4 2.9 2.4 38-47 7.3	INTERVAL N 1-17 18-25	UMBERS % TO 0.6 1.3 2.3 2.3	OFAL RE OCCURING IN	ERCH INTERVAL
5.4 35 2.9 2.4 38:47 7.3	INTERVAL N 1-17 18-25	UMBERS % TO O.6 1.3 2.3 2.3 5.4		ERCH INTERVAL
35 2.9 36=37 2.4 38=47 /.3	INTERVAL N 1-17 18-25	UMBERS % TO O.6 1.3 2.3 2.3 5.4 7.8		ERCH INTERVAL
>6-37 2.4 	INTERVAL N 1-17 18-25	UMBERS % TO O.6 1.3 2.3 2.3 5.4 7.8 32.8		ERCH INTERVAL
7.3	INTERVAL N 1-17 18-25	UMBERS 9,0 TO O.6 1.3 2.3 2.3 7.8 32.8 5.4		EACH INTERVAL
	JNTERVAL N 1-17 18-25 26-29 30 31 32 33 34	UMBERS 90 TO 0.6 1.3 2.3 2.3 5.4 7.8 32.6 5.4 2.3		ERCH INTERVAL
42-48	JNTERVAL N 1-17 18-25 26-29 30 31 32 32 34 35 36-37	UMBERS % TO O.6 1.3 2.3 2.3 5.4 7.8 32.8 5.4 2.3		ERCH INTERVAL
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	JNTERVAL N 1-17 18-25 26-29 30 31 32 32 34 35 36-37	UMBERS 9,0 TO O.6 1.3 Z.3 Z.3 7.8 32.6 5.4 2.9 1.3		EACH INTERVAL
	JNTERVAL N 1-17 18-25 26-29 30 31 32 32 34 35 36-37	UMBERS 9,0 TO O.6 1.3 Z.3 Z.3 7.8 32.6 5.4 2.9 1.3		ERCH INTERVAL
	JNTERVAL N 1-17 18-25 26-29 30 31 32 32 34 35 36-37	UMBERS 9,0 TO O.6 1.3 Z.3 Z.3 7.8 32.6 5.4 2.9 1.3		EACH INTERVAL
	JNTERVAL N 1-17 18-25 26-29 30 31 32 32 34 35 36-37	UMBERS 9,0 TO O.6 1.3 Z.3 Z.3 7.8 32.6 5.4 2.9 1.3		ERCH INTERVAL
	JNTERVAL N 1-17 18-25 26-29 30 31 32 33 34 35	UMBERS 9,0 TO O.6 1.3 Z.3 Z.3 7.8 32.6 5.4 2.9 1.3		ERCH INTERVAL

MICHAEL	BAKER,	JR.,	INC.
1			

THE BAKER ENGINEERS

Subject DORCIS CREEK DAM S.O. No. 100- YEAR DICKAPESE CHLCULATION Sheet No. 7 of 12

Box 280 Beaver, Pa. 15009

__ Drawing No. ____ Computed by GWT Checked by Will Date 11-26-80

THE INFLOW TO THE IMPOUNDMENT FOR THE 100-YEAR FLOOD WAS CALCULATED USING MATERIAL FROM "THE HYDROLOGIC STUDY - TROPICAL STORM AGNES" PREPARED BY THE SPECIAL STUDIES BRANCH, PLANNING DIVISION, NORTH ATLANTIC DIVISION, CORPS OF ENGINEERS, IN NEW YORK CITY.

DRPINAGE AREA - 7.77 SQ MI

O COMPUTE THE MEAN LOGARITHM

LOG (an) = Cm + 0.75 LOG A

LOG (97) = MEAN LOGARITHM OF ANNUAL FLOOD PEAKS

A: DRAINAGE AREA, SQ. MI = 7.77 Sq. M.

C. : MAP COEFFICIENTS FOR MEAN LOG OF ANNUAL PEAKS FROM FIG. 21 = 2,15

LOG (9m) = 2,15 + 0.75 (LOG 7.77)

= 2.818

(2) COMPUTE STANDARD DEVIATION

S = C, -0.05 (LOGA)

S: STANDARD DEVIATION OF THE LOGARITHMS OF THE ANNUAL PEAKS.

C5 = MAP COEFFICIENT FOR STANDARD DEVIRTION FROM F16. 22 = 0.349

A = DFAINAGE AREA, Sq. MI. = 7.77 Sq. M.

5 = 0.349 - 0.05 (LOG 7.77)

= 0.305

- (3) SELECT SKEW COEFFICIENT FROM FIG. 23 =+0,20
- **(4)** 109 (9,00) = 109 (9,00) + K(P,0) 5

K.(P.g) : STANDARD DEVIATE FOR A GIVEN EXCEEDENCE FREQUENCY PERCENTAGE (P) AND SKEW COEFFICIENT (9) FROM EXHIBIT 39 OF BEARD'S "STATISTICAL METHODS IN HYDROLOGY "

LOG (9,00) = 2,8/8 + 2,48 (0,305)

Q100 = 3,755 CFS

USING THE SNYDER'S UNIT HYDROGRAPH PARAMETERS DEFINED FOR THIS BASIN PRODUCED A PEAK FLOW OF 3690 CFS. THIS VALUE IS WITHIN 2 % OF THE PREVIOUSLY COMPUTED PEAK FLOW OF 3755 CFS AND IS WITHIN THE 10% LIMIT SUGGESTED BY CORPS GUIDLINES.

0.006 1083-4 1084-2 1064-9 1085-4 1080-1 1080-9 1081-0 1080-1 537-08 1047-29 1664-92 2369-06 3100-36 3960-10 4882-21 5899-01 18-34 59-18 0.013 000.0 4242 4-0.013 0.000 RAIVO OF 100-YEAR FLOOD HATIUNAL PRUGRAA FUR INSPECTION UF NON-FEDERAL DAMS HYDRULIC AND HYDRALIC AND HYDRALIC AND METHOD UNIT HYDRUGRAPH BY SNYOEKS METHOD 3.024 0.000 220 220 224 1087.0 1089.0 3.006 210 0.003 RUJI ING FUR DUBUIS CREEK UAM 0.006 0.054 321 RU LIFE HYDRUGRAPH TO DAM 1086.0 3.030 0.000 3.030 0.000 3.030 0.013 3.033 0.006 3 1085.8 1982.1 79.0 1032 2.83 0 < 1 1.185.6 **در ۱۰**۰۰ ELJUD HYDRDURAPH PALKAGE I HEL-11 DAM SAFETY FESTUN JULY 1978 LAST 4001FICATION 26 FEB 79 MBJ UPDATE 11 0.035 11 0.036 11 0.036 11 0.054 11 0.013 3.14 \$E 1075 \$\$1082-0 \$01035-4 \$L 0 30, 7501 ¥ % ¥

66.3. ******** AUTO x 3 LINAME LOTAGE AV I VA - X C#51L ******** -0.35 KILOR Z.OU MATTU ASNUM HATEENAL PROGRAM FOR EN PROCEEDING OF HON-FOOTMAL DAMS MYDROLDIEL AND HYDRAULICEAMALYSES—OF DUBUIS ENELS DAM MITE HYDROGRAPH BY SNYOLRS METHOD 141 AGG ULIKE KIIGE EKAIN DIKKA KIIUK SIKIE 0.0 1.00 0.0 1.30 1.00 MULTI-PLAY ANALYSES TO BE PERFURMED NPLAYE I ANTIOF I ENTIOF I UATE HYBRUSKAPH DATA

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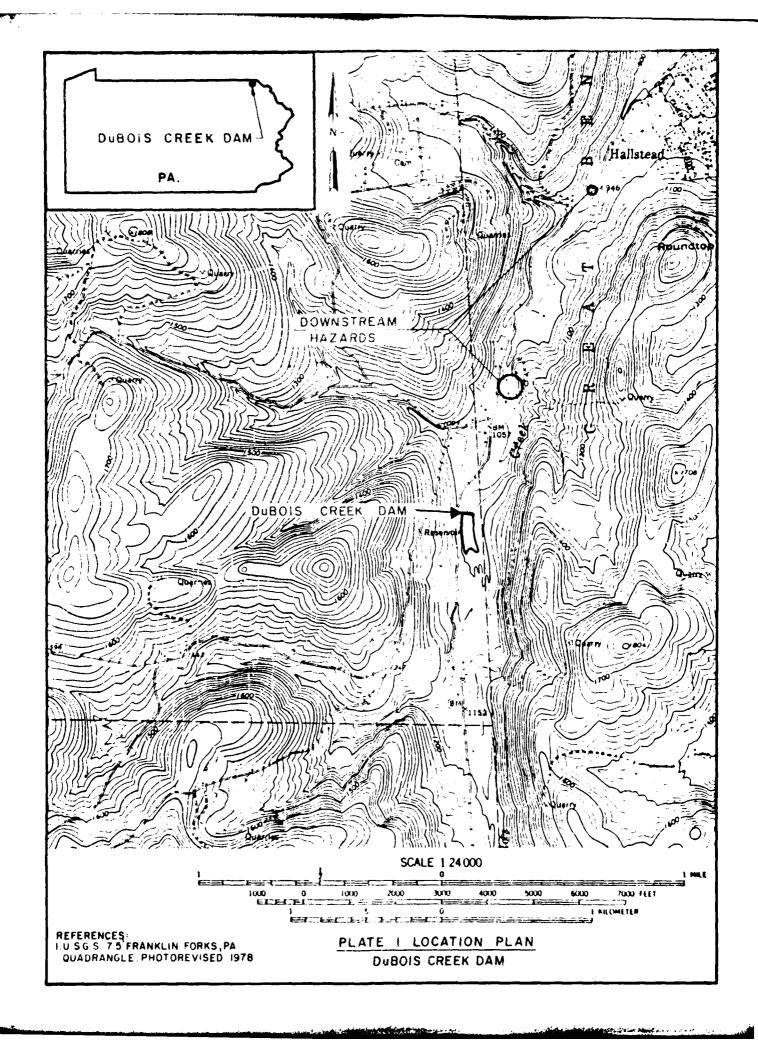
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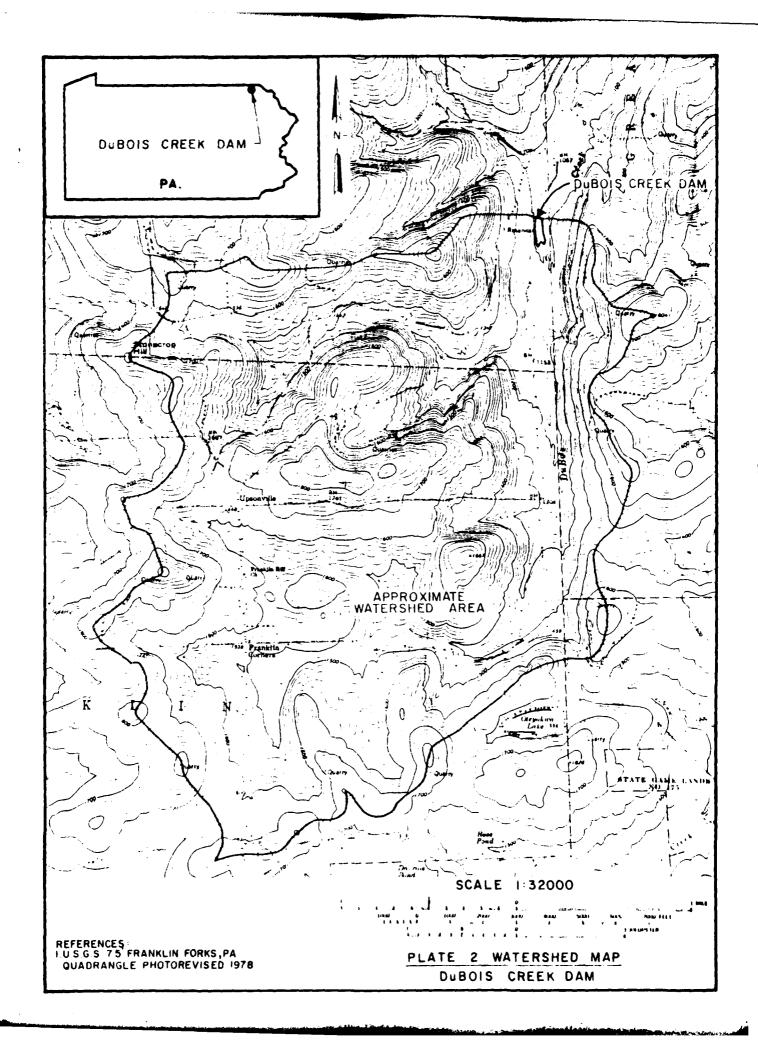
APPENDIX E

PLATES

CONTENTS

- Plate 1 Location Plan
- Plate 2 Watershed Map
- Plate 3 Profile and Plan of Dam (1919)
- Plate 4 Reconstruction Drawing of Right Spillway Training Wall (1930)
- Plate 5 Plan, Profile, and Cross Section of Dam (1905)





ELEVATION

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PLAN Scale 110 - 1"

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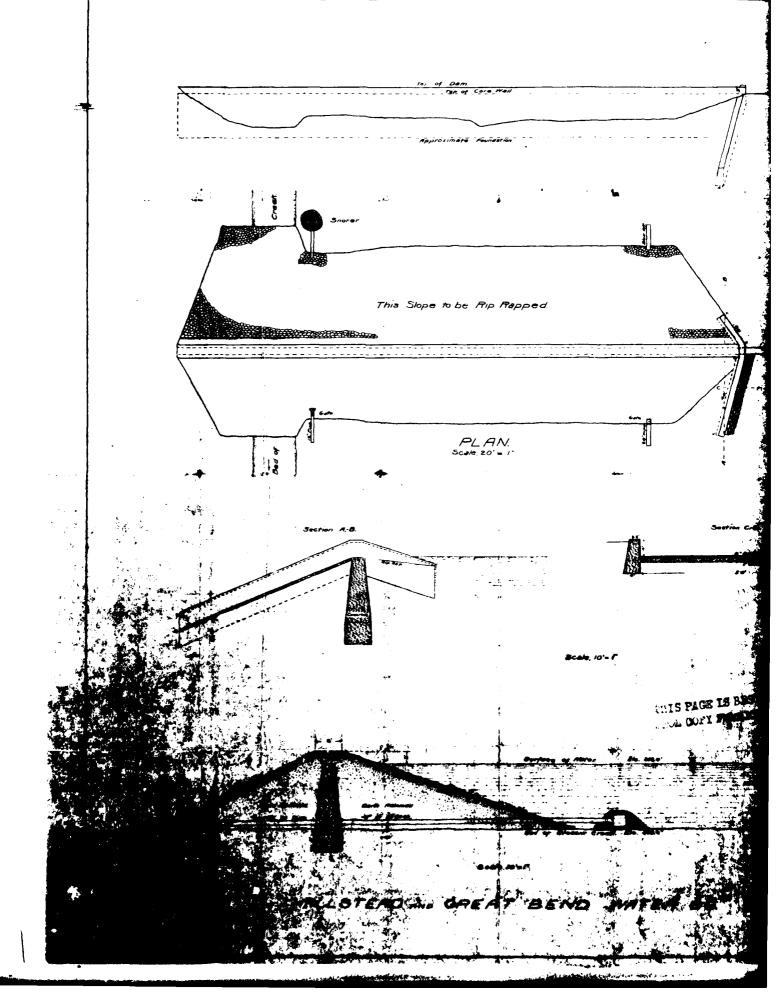
PLATE - 3

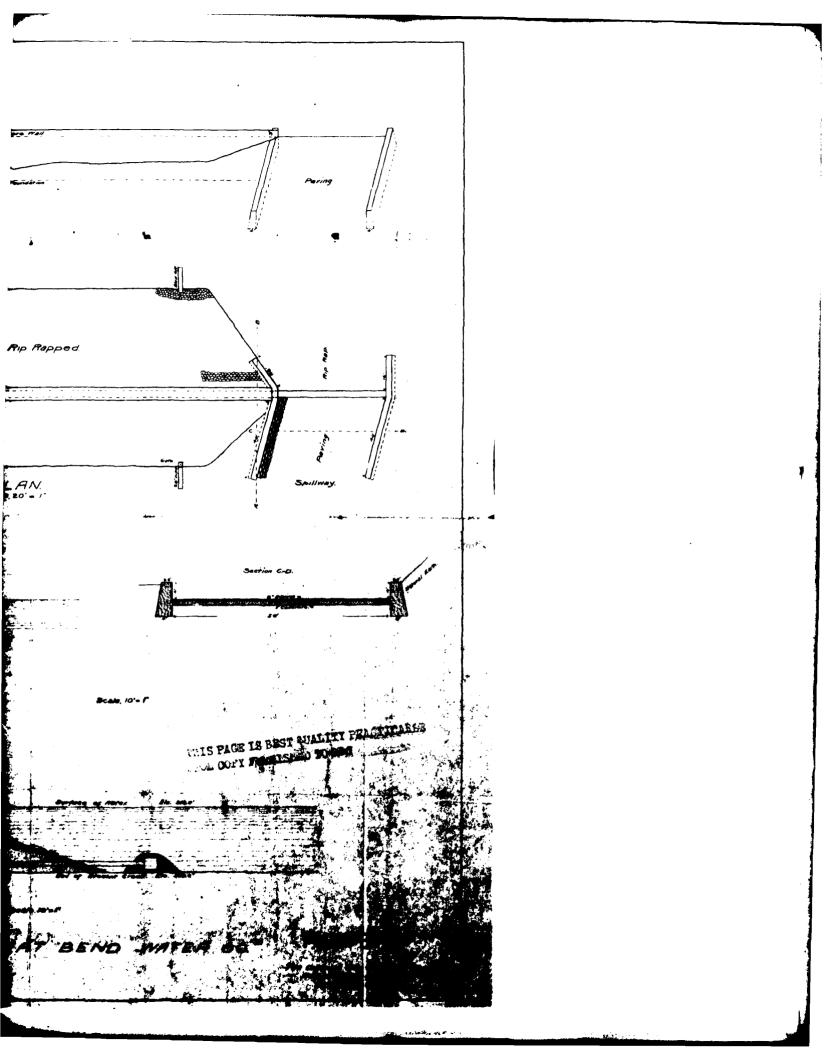
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54'-0" This Porting Rebuilt , 937 35-0 Bottom of Spillmay Channel Goucrete with one raph stone Rubble-Mason

24-0" Existing Wall Rebuilt 1926 or 1927 Buit or Stone Filled French PLAIT Scar & 1-0" ulthroy Channel --ELEVAT ON Elettom of Spiling Channel o boles spaced every 10 FL Goocrete with





APPENDIX F

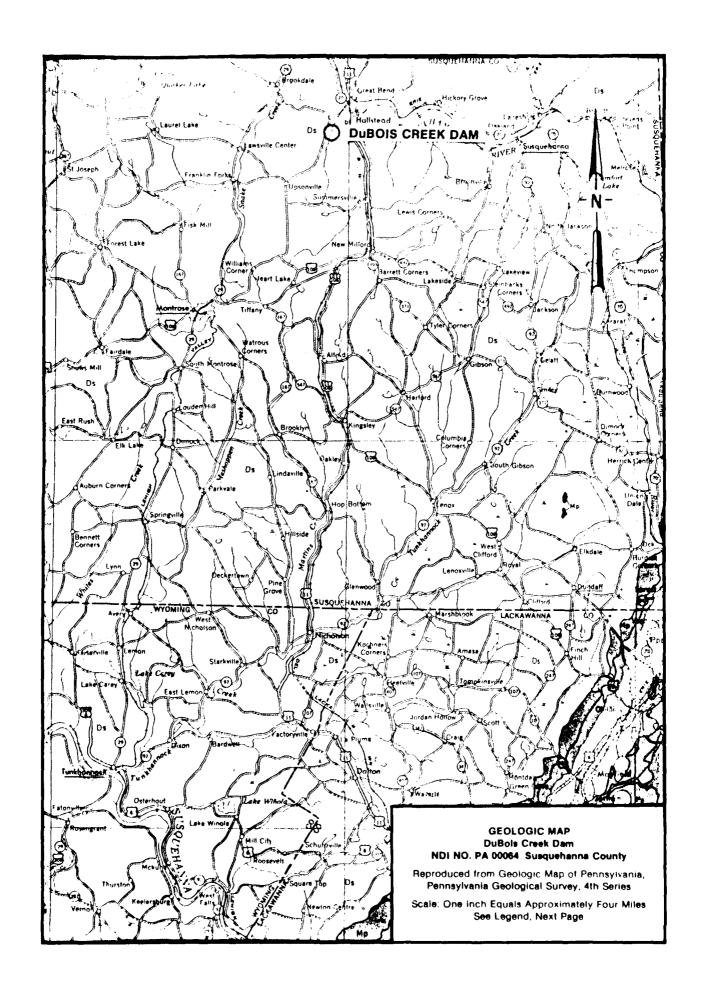
REGIONAL GEOLOGY

DuBOIS CREEK DAM NDI No. PA 00064, PennDER No. 58-8

REGIONAL GEOLOGY

DuBois Creek Dam is in a steep walled valley located in the Glaciated Low Plateaus physiographic province. The area has undergone glaciation at least three times and is presently covered with Wisconsin Stage glacial deposits. According to the Soil Conservation Service's Soil Survey for Susquehanna County, the surface soils consist primarily of very stoney, silt loams of the Mardin-Volusia-Oquaga association. No test boring data were available for review, thus, the thickness of this overburden is difficult to ascertain.

Geologic references indicate bedrock in the vicinity of the dam to be composed of the lower members of the Catskill Formation and the upper members of the Chemung Formation; both belonging to the Susquehanna Group. The dam lies near the contact between the Catskill, which outcrops in the upper reaches of the valley as red and gray shales and sandstones, and the Chemung, which underlies most of the valley floor downstream of the dam. The Chemung Formation consists of prodelta, fossiliferous, gray, sandy shales and gray to olive green sandstones of Upper Devonian age. A bedrock sample obtained from the valley floor downstream of the dam was a hard, olive green fine to medium grained sandstone, probably of the Chemung Formation. The strata underlying the dam may be dipping slightly to the southeast on the southern limb of the Rome Anticline which extends northeast from Friendsville and fades out near Hallstead.



GEOLOGY MAP LEGEND

DEVONIAN UPPER

WESTERN PENNSYLVANIA



Oswayo Formation

CISWAYO FORMATION

(prenish gray to gray shites, sittstones and
sond-course becoming increasingly shillo
worstward, considered equivalent to type
Osciago Kievville Formation Dr in Eric
and Crawford Counties probably not
distinguishable north of Corry



Cattaraugus Formation

s access augus Formation
Red, gray and brown shale and sandstone
with the proportion of red decreasing wist
wided to indice Venings sands or didlers
and Salamanea sandstone and complomer
are, some limestone in Crawtord and Evic
country.



Conneaut Group

Mitrauting gray, brown, greenish and purptish shales and sitistones, includes "pink rock" of drillers and "Chemung" and "Giraid" Formations of northwest-ern Pennsylvania.



Canadaway Formation

Alternating brown shales and sandstones, includes "Portage" Formation of north-western Fernagivania.



Oswayo Formation

CISMBYO FORTHBLION
Brownish and greenish gray, fine and
neckism grained sounds nees with some
shies and southered centariesus lenses
includes red shales which become more
numerious enabourd. Relation to type
Oswayo not proved.

CENTRAL AND EASTERN PENNSYLVANIA



Catskill Formation

CRISKIII FORMATOR
Cherily red to brownish shales and sand-stones includes gray and greenish sunt-stone tongues named Elk Mountain, Honesalae Shohola, and Delaware River in the east.



Marme beds

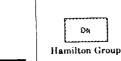
maine ocus
Gray to alive brown shales, graywackes,
and sandstones, contains "Chemany" beds
and "Portoge" bids including Burkel,
Braffer, Hurrell, and Trimmers Rock,
Tuly Limistone at base



Susquehanna Group

Barbed line is "Cheminy-Catshill con-tact of Second Pennsylvania Survey County reports barbs on Cheminy side of line





Mahantango Formation

meanium to alive shale with interbedded sandstones which are dominant in places (Montrbello), highly Jossitterous in upper part, contains "Centerfield coral bed" in castern Pennsylvania.



Black, Insule, carbonaceous shale with thick, brown sandstone (Turkey Ridge) in parts of central Pennsylvania.



Onondaga Formation

Onondaga Formation (irrenish bine, thin bedded shale and dark bine to black, medium bedded itmestone with shale predominant in most places, includes Stinsarove Lunestone and Needmore Shale in central Pennsylvania and Buttermith Falls Limestone and Esopus Shale in sasternmost Pennsylvania, in Lehija Gup area includes Palmerton Sandstone and Bowmanstown Chert





Oriskany Formation

White to brown, I see to course grained, partly calcurous, locally conglowerstro, fossilterons sandstone Religiely at the top, dark gray, cherly timestone with some interbedded shales and sandstones below (Shriver).



Helderberg Formation

Dirk gray, culcurous, thin bedded shale (Mandata) at the top, equivalent to Port Econ Shale and Herratt Limestone in the east dark gray, cherty, thin bedded, fossiliterous timestone (New Scotland) with some local sandstones in the middle ond, at the base dark gray, medium to thick bedded, crystalline limestone (Cogmans, sandy and shaly in places with some shirt modules.



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